

Didymos Binary System Dynamics & Physical Properties Investigations for the DART Mission

Including Outcomes of the DART Impact

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Goddard Space Flight Center
Johnson Space Center
Langley Research Center
Glenn Research Center
Marshall Space Flight Center
Planetary Defense Coordination Office





Jet Propulsion Laboratory California Institute of Technology







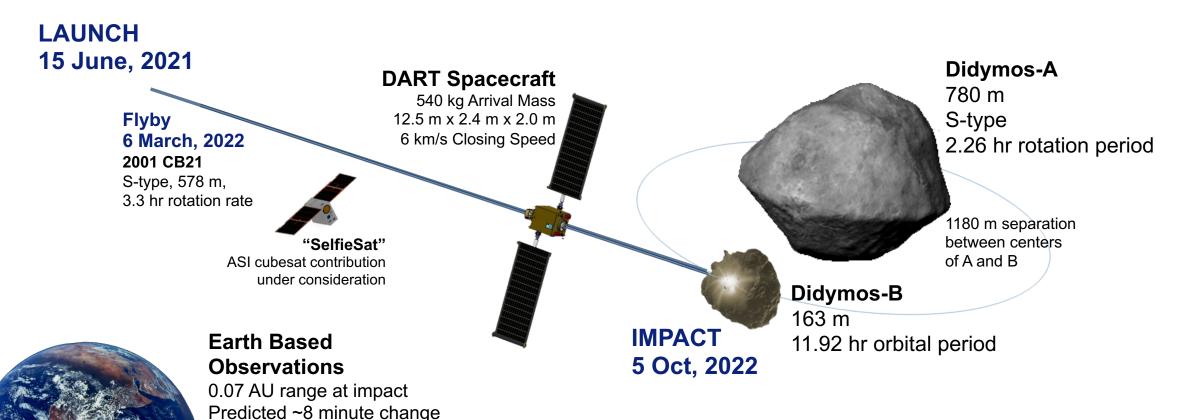
Double Asteroid Redirection Test (DART)

- Designed to be first meaningful demonstration of kinetic impactor
- Target the binary NEA system 65803 Didymos (1996 GT)
- Impact Didymos-B and change the period of mutual orbit
- Measure the period change from Earth-based assets

in binary orbit period

Recent Mission Milestones:

- DART Investigation Team Meeting held: 9 April, 2018
- PDR completed: 10–12 April, 2018
- KDP-C: 10 July, 2018

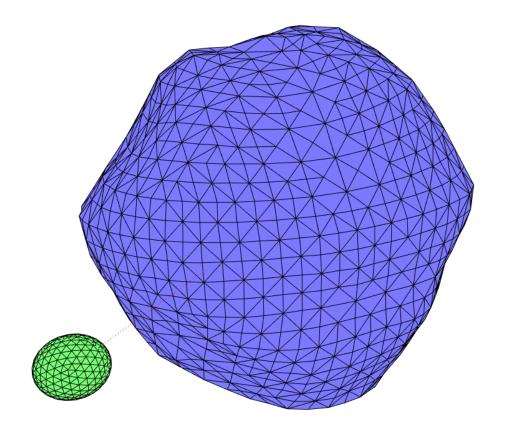




Dynamical & Physical Properties Working Group

Many Ongoing Studies with these Objectives:

- 1) Characterizing the Didymos system's preimpact dynamics, and un-perturbed and perturbed time evolution thereof, consistent with all observation data
- 2) Modeling changes to the system's dynamics that may be induced by the DART spacecraft's impact
- Determining how physical properties can be inferred based on current knowledge

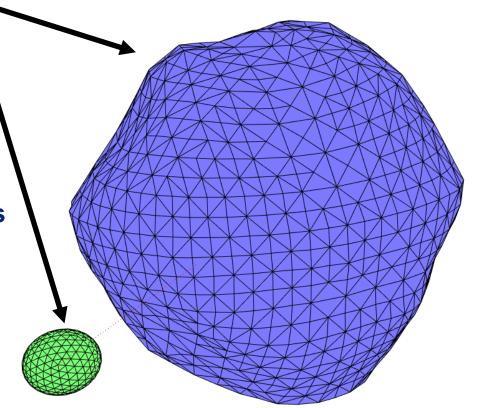




Didymos Reference Model (DRM)

Key Features of System

- Radar and light curve derived primary shape model
- Can only assume axial ratios for elongated ellipsoidal secondary ($a_s > b_s > c_s$; $a_s/b_s = 1.3 \pm 0.2$; $b_s/c_s = 1.2$)
 - available data don't support getting secondary shape
- Primary rotation period and binary orbit period well constrained from photometric light curve data
- From mean separation and orbit period, get system mass
- Individual component masses not yet distinguished!
- Derived bulk density (assumed common) has large uncertainty
- Assume on-average synchronous rotation of secondary
- Assume near-alignment of both body spin poles with orbit pole





Didymos Reference Model (DRM)

Key Features of System

Parameter Value		Parameter	Value
Primary rotation period	$2.2600 \pm 0.0001 \mathrm{hr}$	Bulk density, ρ	2104 kg/m ³ ±30%
Mutual orbit period	11.920 + 0.004/-0.006 hr	System absolute magnitude, H	18.16 ± 0.04
Mean separation, a_{orb}	1.18 + 0.04 / -0.02 km	Geometric albedo	0.15 ± 0.04
Total system mass	$5.278e11 \pm 0.54e11 \text{ kg}$	Radar albedo	$0.27 \pm 25\%$
Diameter ratio, D_S/D_P	0.21 ± 0.01	Mutual orbit eccentricity	$e \le 0.03$
Primary Diameter, D_P	780 m ± 10%	Mutual orbit pole (ecliptic lon.)	$\lambda = 310^{\circ}$
Secondary Diameter, D_S	163 ± 18 m	Mutual orbit pole (ecliptic lat.)	$\beta = -84^{\circ}$

Note: Observations planned for March 2019 apparition should, if successful, eliminate current uncertainty about secondary elongation, and establish (so far assumed) synchronous rotation of secondary



Didymos Reference Model (DRM)

Key Features of System

Parameter Value		Parameter	Value
Primary rotation period	2.2601 ± 0.0001 hr	Bulk density, ρ	2104 kg/m ³ ±30%
Mutual orbit period	11.92164 ± 0.00003 hr **	System absolute magnitude, H	18.16 ± 0.04
Mean separation, a_{orb}	1.18 + 0.04 / -0.02 km	Geometric albedo	0.15 ± 0.04
Total system mass	$5.278e11 \pm 0.54e11 \text{ kg}$	Radar albedo	$0.27 \pm 25\%$
Diameter ratio, D_S/D_P	0.21 ± 0.01	Mutual orbit eccentricity	$e \le 0.03$
Primary Diameter, D_P	780 m ± 10%	Mutual orbit pole (ecliptic lon.)	$\lambda = 270^{\circ}$
Secondary Diameter, D_S	163 ± 18 m	Mutual orbit pole (ecliptic lat.)	$\beta = -87^{\circ}$

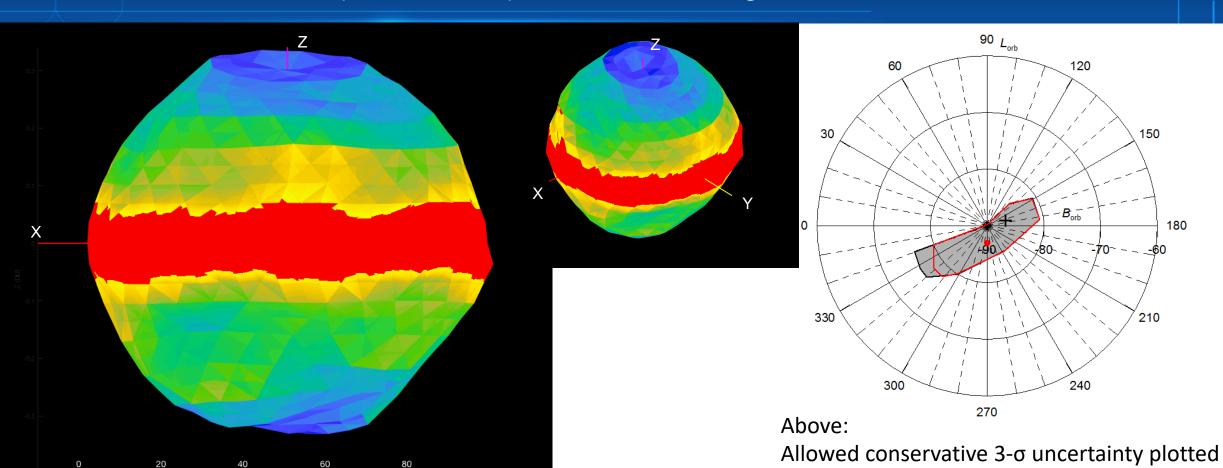
Recent changes suggested at June 2018 Didymos Observers workshop in Prague

** Assuming zero BYORP! But 5 possible BYORP ΔM solutions exist, one of them consistent with zero, and 2019 + 2020/2021 apparition observations should be capable of distinguishing between them!

Primary Near Spin Disruption Limit?

Net Accel. Slope (deg.)

Local Acceleration Slope on Primary Surface, assuming DRM nominal values:



Black outline: 2003+2015 data

Red outline: 2003+2015+2017 data

Long-Term Time Evolution of Pre-Impact Dynamics

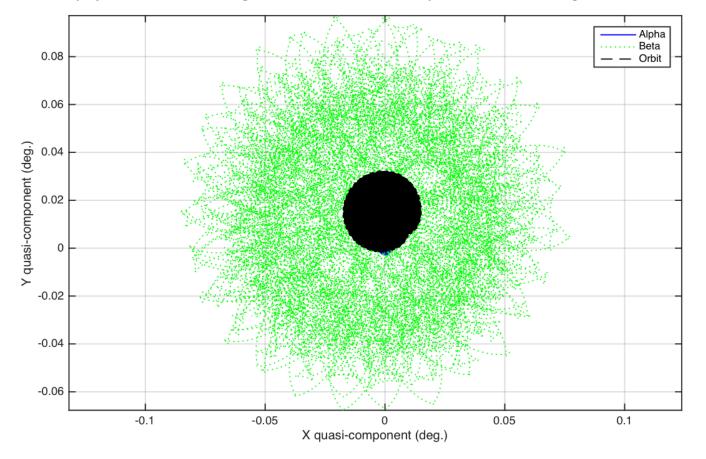


- External tides from Sun and Planets
- Solar radiation pressure
- Thermal re-radiation (B-YORP)
- Inter-component tidal energy dissipation



- Example Didymos instantiations consistent with DRM
- Observe expected modes of motion:
 - Body spin and orbit angular momenta vectors co-precession

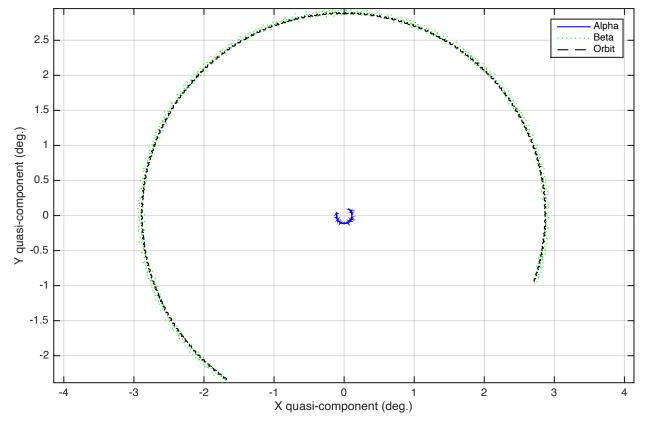
Quasi-projection of normalized angular momentum vectors onto plane normal to total angular momentum vector





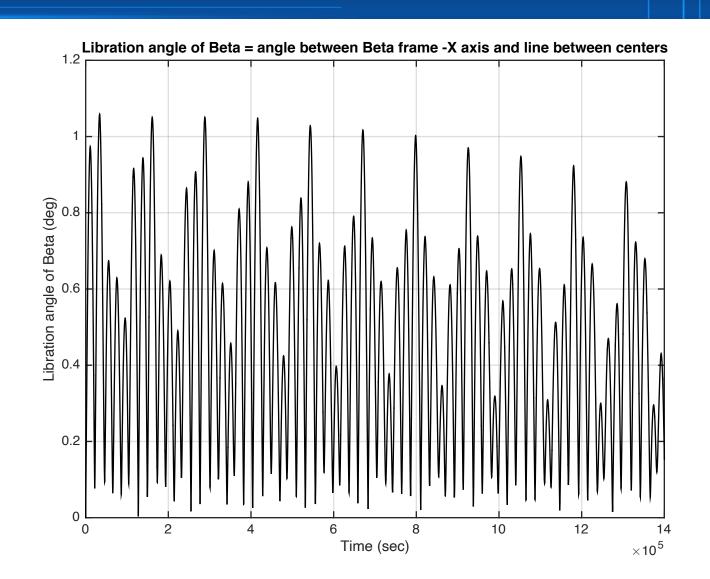
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Quasi-projection of normalized angular momentum vectors onto plane normal to total angular momentum vector

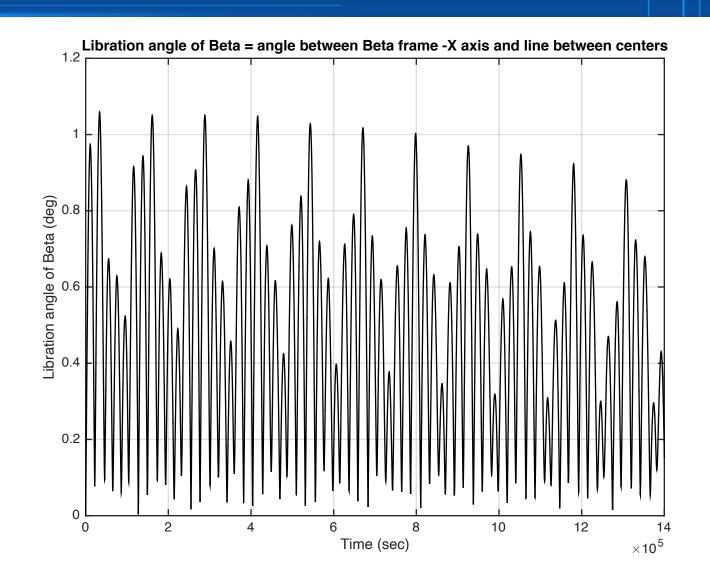




- Example Didymos instantiations consistent with DRM
- Observe expected modes of motion:
 - Body spin and orbit angular momenta vectors co-precession
 - Secondary libration



- Example Didymos instantiations consistent with DRM
- Observe expected modes of motion:
 - Body spin and orbit angular momenta vectors co-precession
 - Secondary libration
- Modes all expected to be as relaxed as possible pre-impact
- Minimum forced libration amplitude → dependent on mutual orbit eccentricity and choice of secondary shape



F2BP Simulation Benchmarking Exercise

Four Test Systems Used



(V=8, F=12) x2

Two Spheres

(V=252, F=500) x2

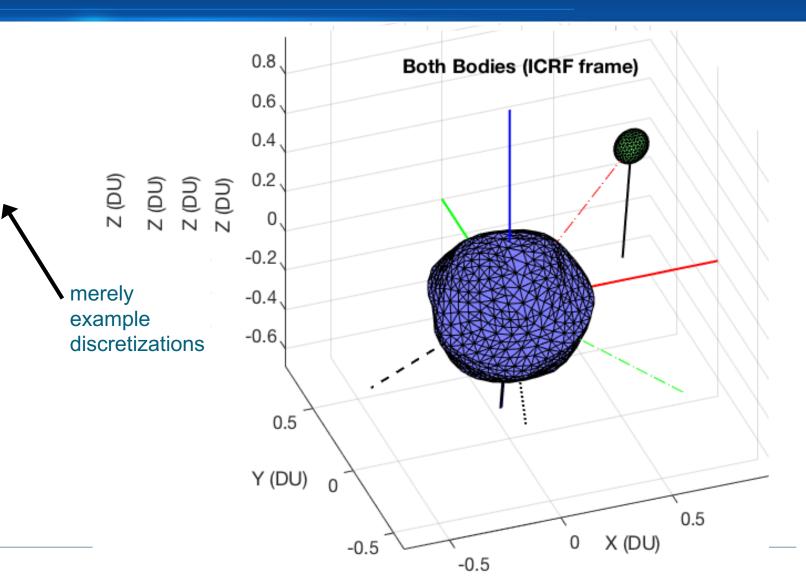
Two Ellipsoids

(V=252, F=500) x2

Didymain shape model + Ellipsoid

> (V=1000, F=1996) x (V=252, F=500)

All systems are "Didymos-like"



F2BP Simulation Benchmarking Exercise

Participants, Methods

Group >>	JPL	GSFC	AU	UCB	UMD
Code description	mutual potential	mutual potential	similar to JPL,	mutual potential	pkdgrav, parallel
	formulation for	formulation for	except uses	formulation using	N-body tree-code
	polyhedra, as in	polyhedra, as in	automatic,	recursive expan-	with mutual
	Werner &	Werner &	recursive order-	sion of inertia	gravity potential,
	Scheeres 2005,	Scheeres 2005,	coefficient	integrals, as in	SSDEM if contact
	relative coord.	inertial coord.	calculator	Hou 2016	forces included
Approach to discretization of shape	tetrahedral	tetrahedral	tetrahedral	polymesh used to	body shapes
	simplex for each	simplex for each	simplex for each	pre-compute	packed with
	polymesh facet	polymesh facet	polymesh facet	inertia integrals	spheres
Free parameters / "knobs"	integration step size, order <i>N</i> of Legendre poly. series expansion	integration step size, but (same) N fixed at $N = 3$	integration step size, order <i>N</i> of Legendre poly. series expansion	integration step size, inertia integral expansion order <i>N</i>	integration step size, kd-tree opening angle, #/size of spheres



F2BP Simulation Benchmarking Exercise

Participants, Methods (Cont'd)

Group >>	JPL	GSFC	AU	UCB	UMD
Scaling of computational cost	$O(n^2)$, $O(6^N)$	$O(n^2)$, $O(6^N)$	$O(n^2)$, $O(6^N)$	only up-front inertia integral calc. is $O(f(N))$	$O(n \log(n))$ with tree-code, $O(n^2)$ w/o using that
Representability of benchmarking models	Two Cubes = exact Two Spheres = approximate Two Ellipsoids = approximate Didymain + Ellipsoid = exact				approximate, except for Two Spheres (in theory)
Numerical integration scheme	2 nd order LGVI, fixed step size = 40s, symplectic, variational, geometric	2 nd order LGVI, fixed step size = 40s, symplectic, variational, geometric	???	RK4, fixed step size = 5s	symplectic 2 nd order leap-frog integrator (fixed step =1.875, 15 s) + adaptive-step RK5
Computer implementation details	written in C, parallelized using MPI, on cluster	FORTRAN, parallelized using MPI, on cluster	C++, not parallelized, single machine	C++, not parallelized, on laptop	written in C, CPU parallelism using pthreads, cluster

Benchmarking Results

Computational Cost

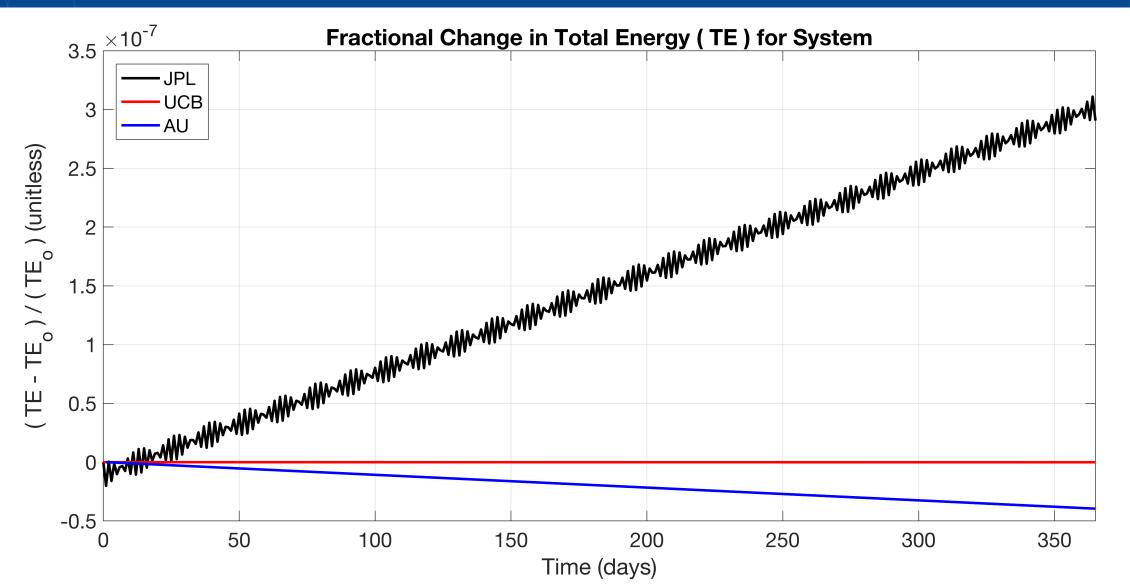
- Sims run for 365+ days
- Sparse-time output every 1 day → leads to peak-shaving, under-sampling for fast angles (libration, etc.)
- Wall-time normalized by duration covered and multiplied by # of processors used = (proc*hrs)/day

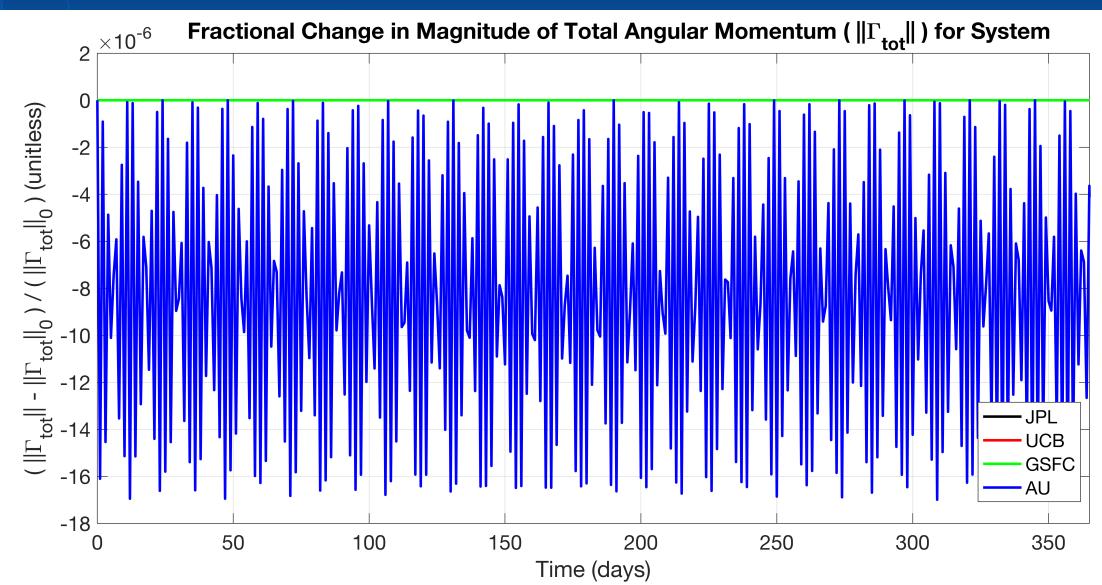
KEY:

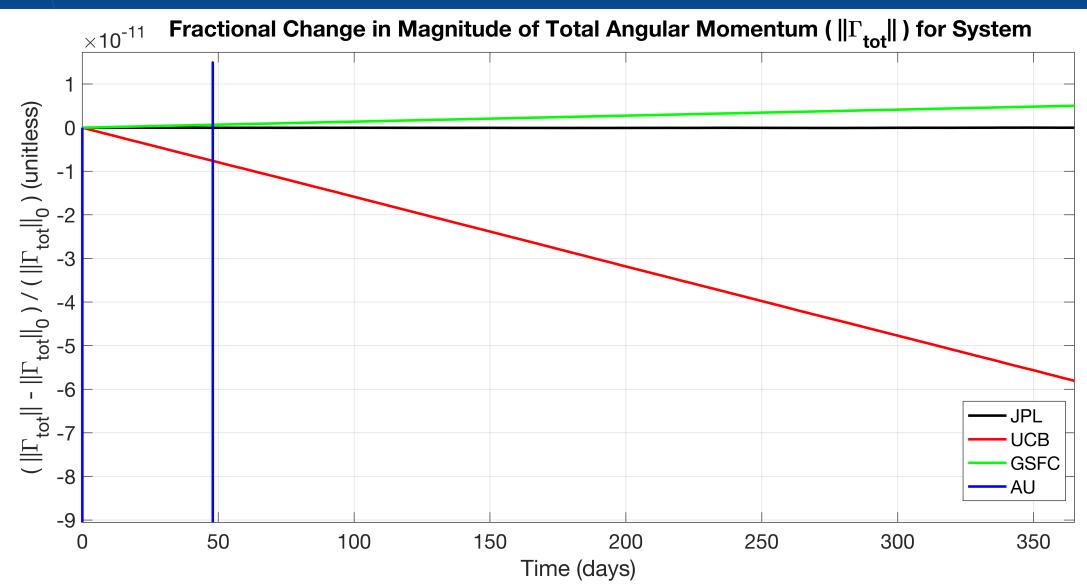
Gravity Order N=3
Gravity Order N=4

Participant	Model 1	Models 2 or 3	Model 4
JPL	~0.017	~3.351	~12.104
UCB	~0.466	~0.466	~0.466
GSFC	~0.081	~5.446	~20.288
UMD			~4.395 , 0.592 *
AU	~0.398 - 0.411		

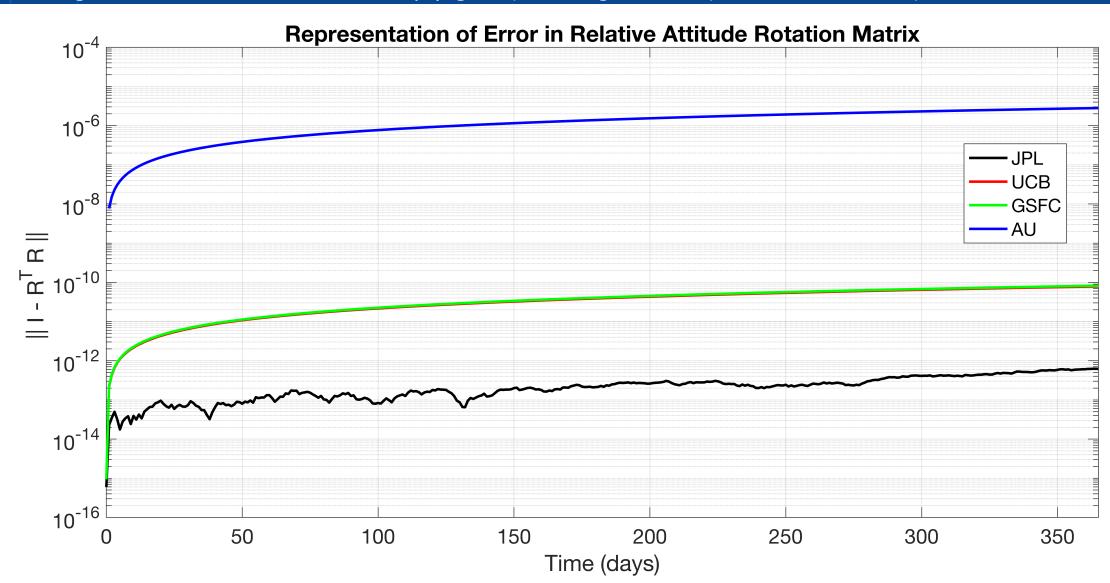




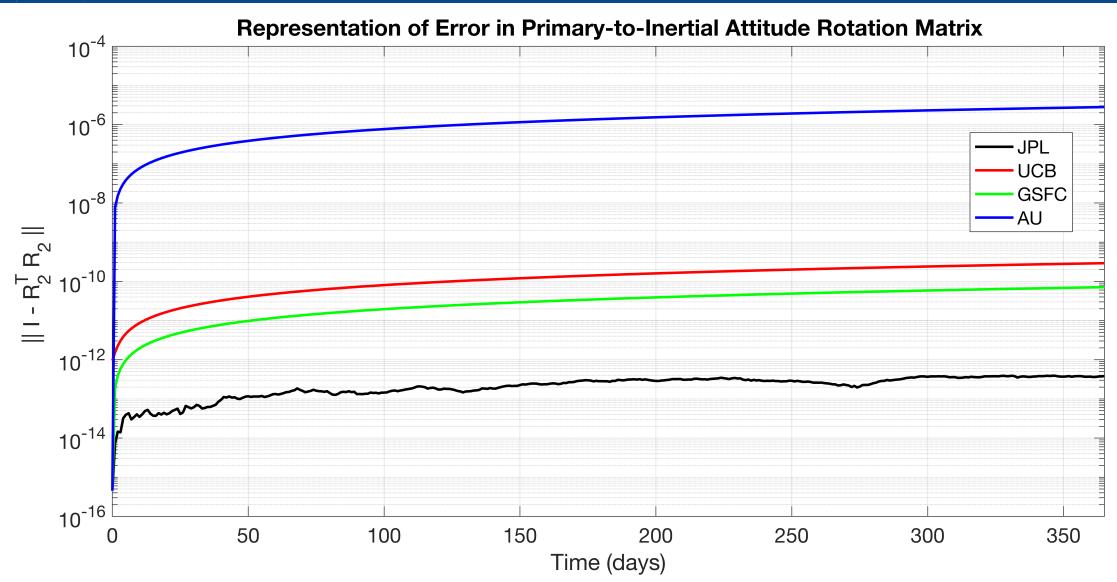




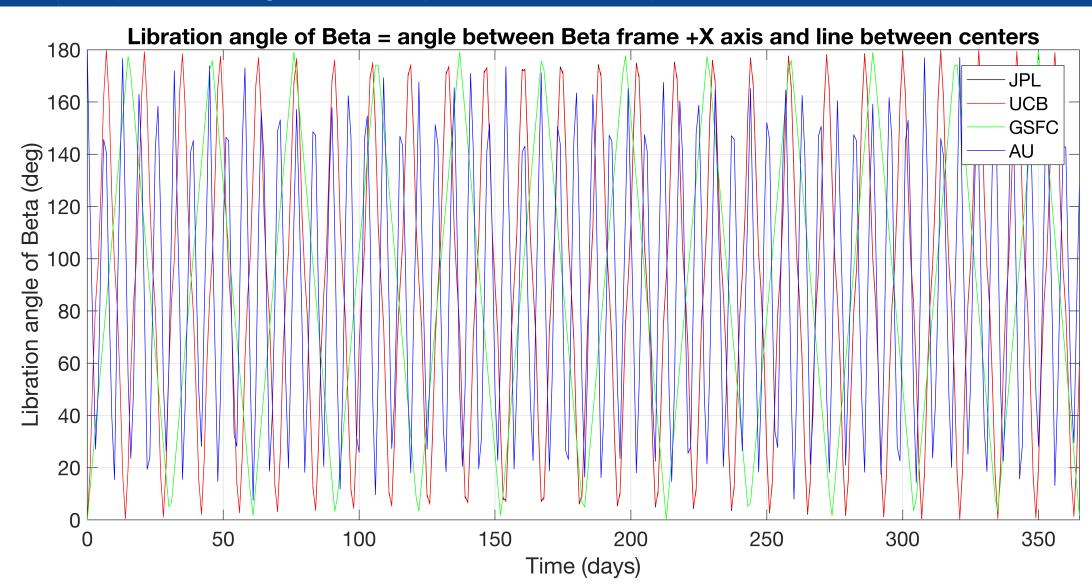
Divergence of attitude from SO(3) group, the geometry of rotational dynamics



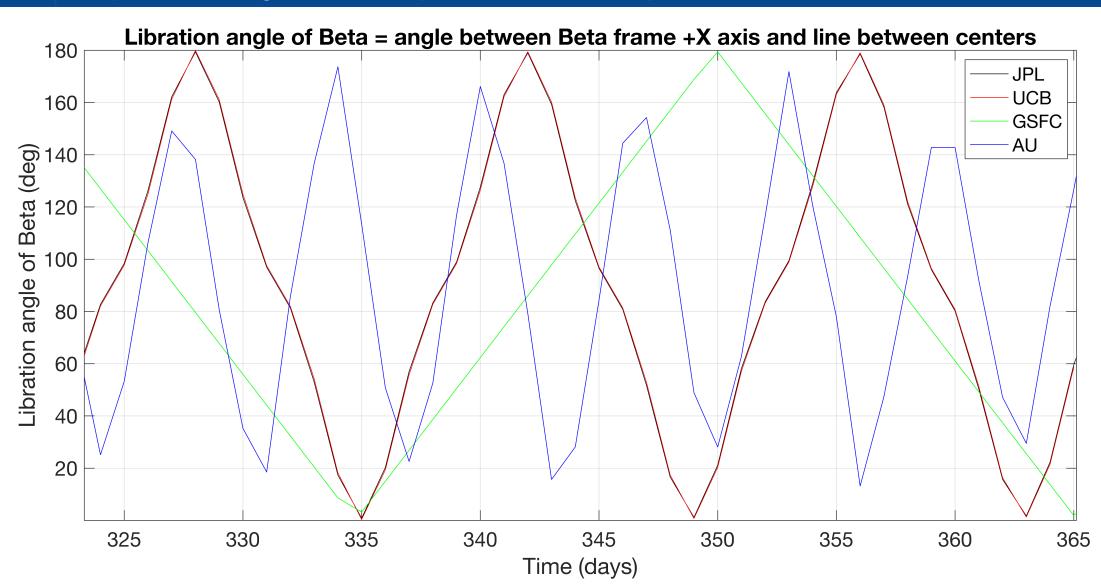
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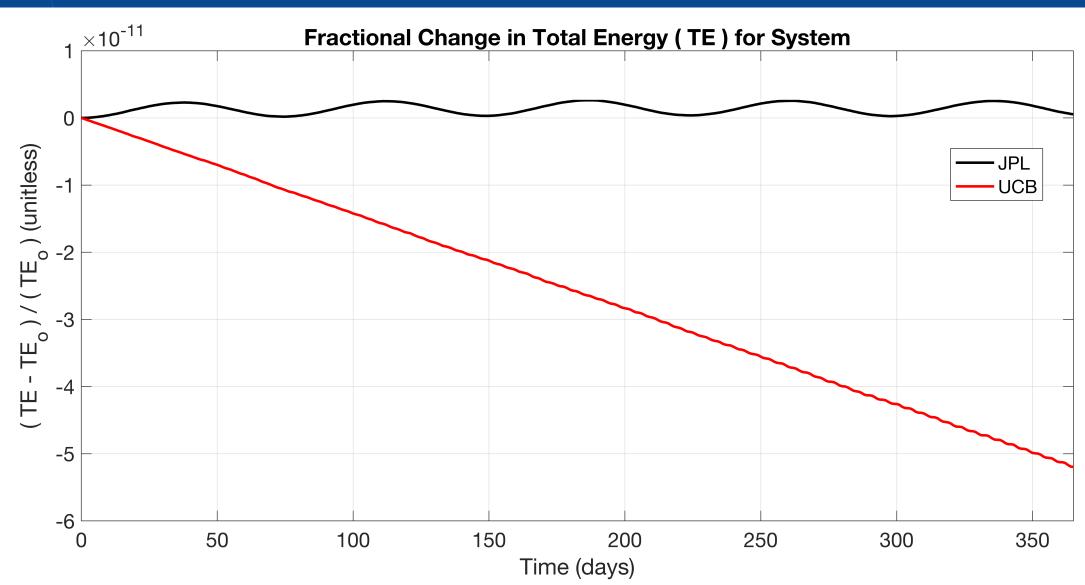
Secondary's initial angular velocity deviation from synchronous -> non-lock, circulation



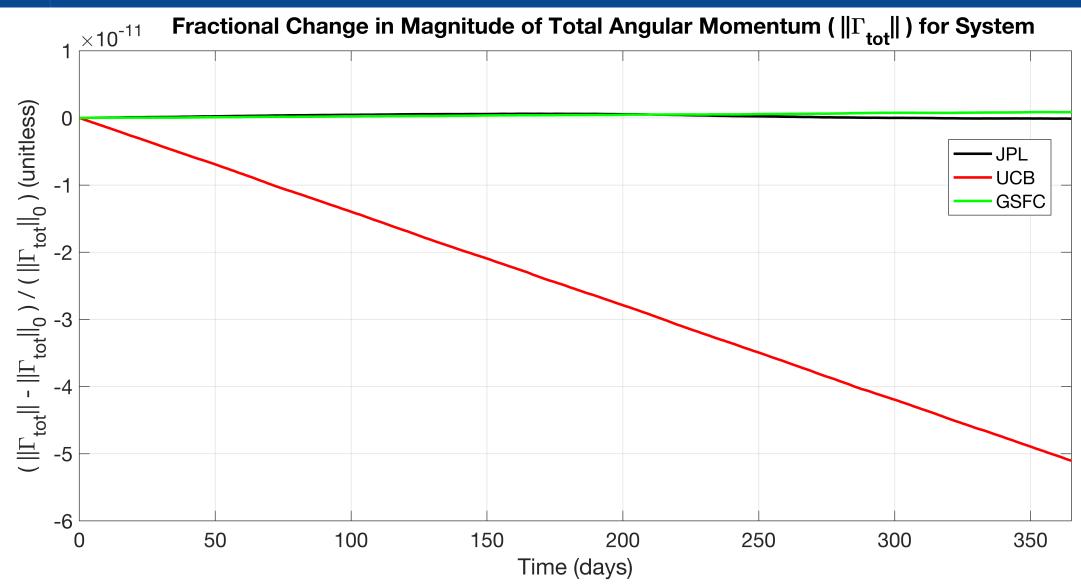
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Benchmarking Results – Two Spheres

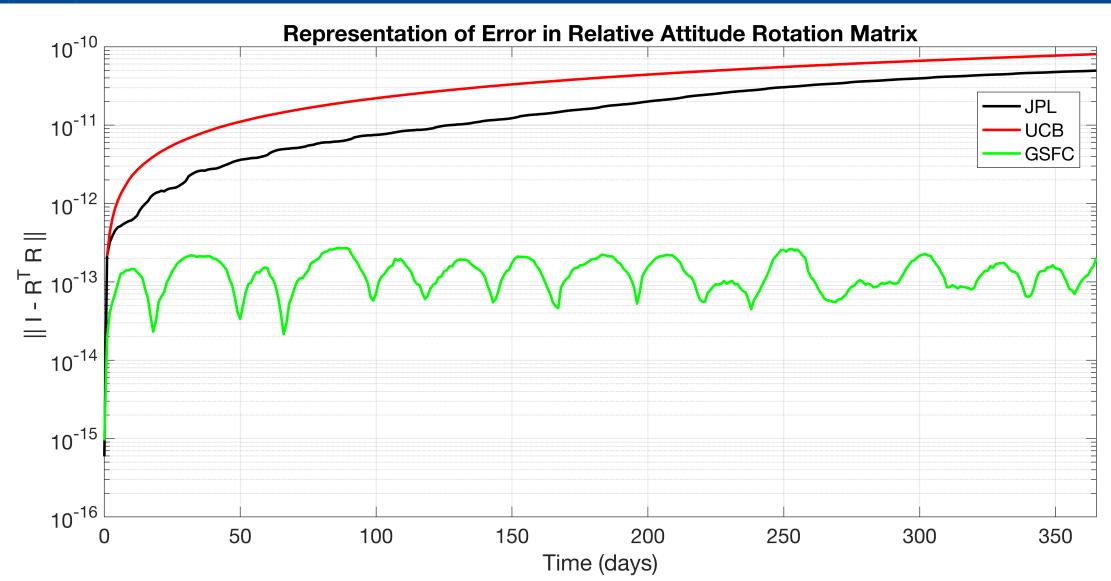


Benchmarking Results – Two Spheres



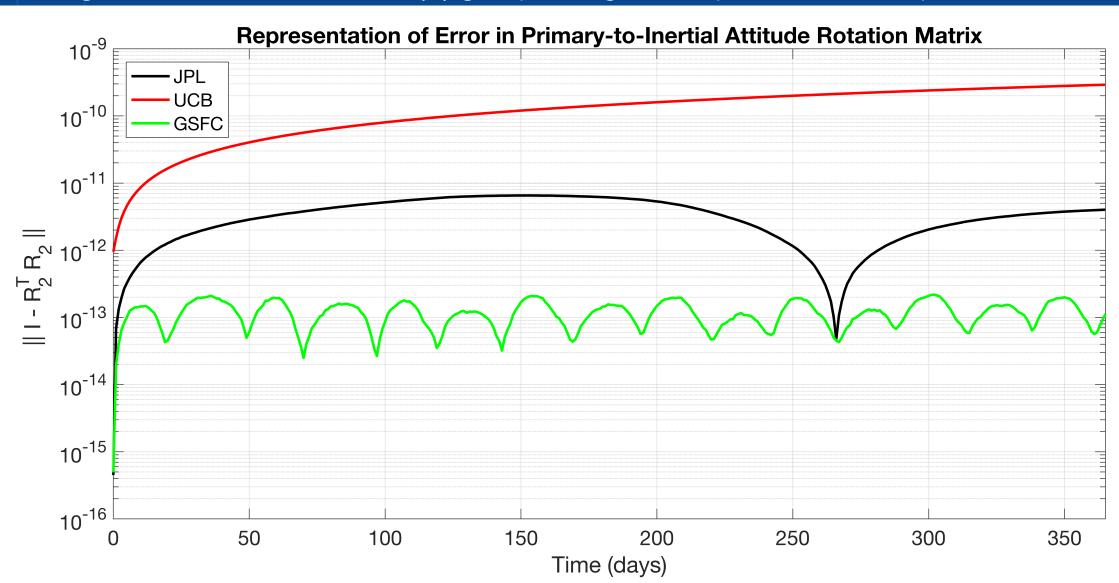
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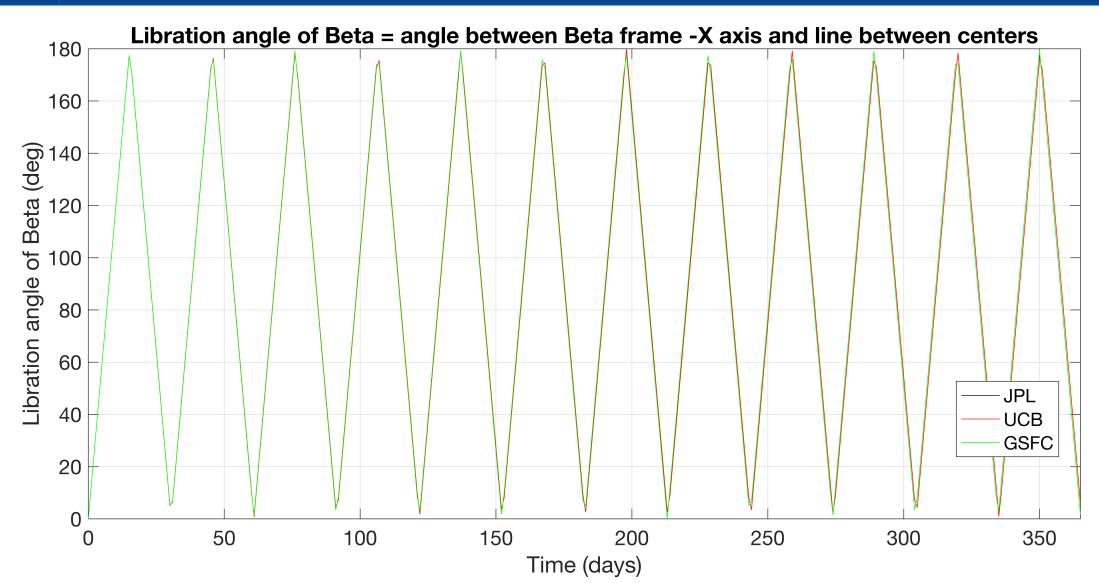
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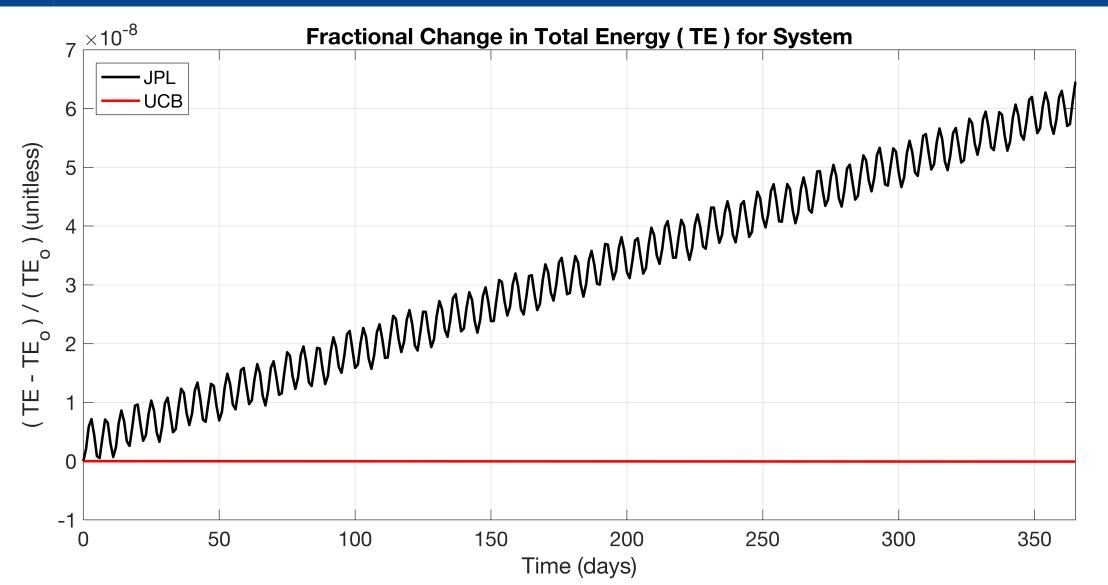
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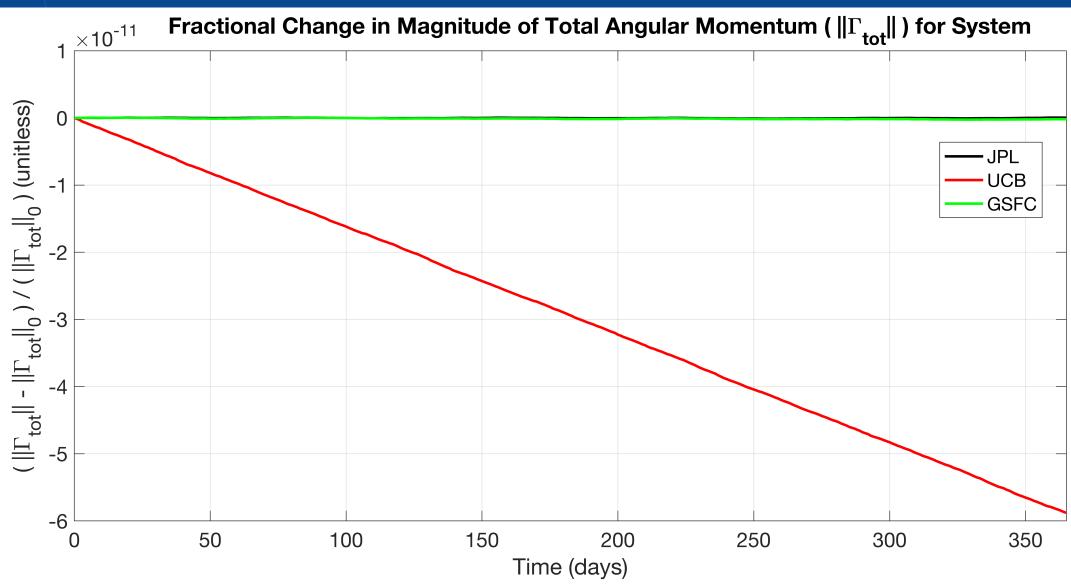


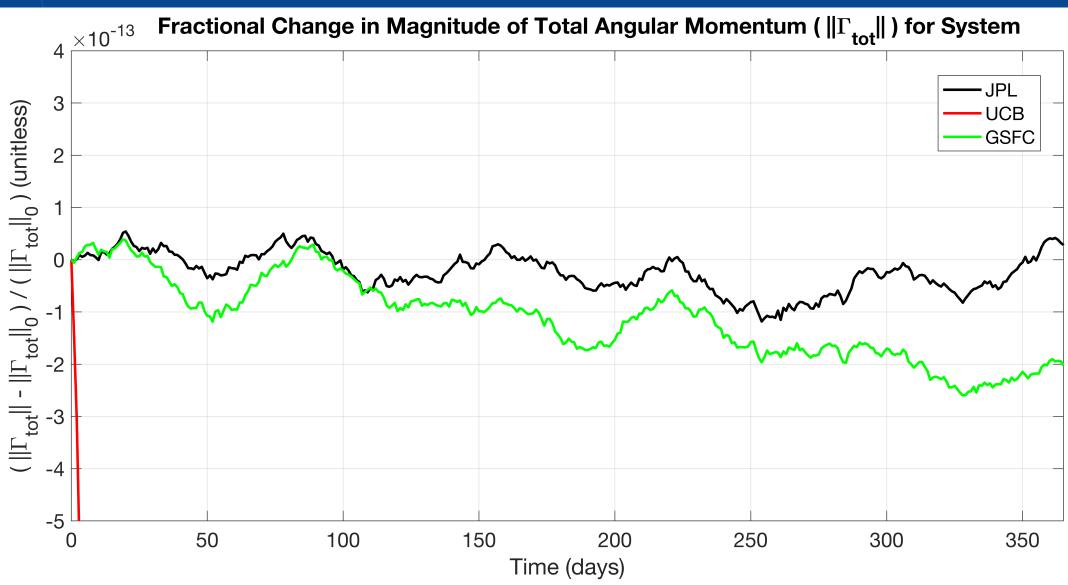
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Secondary's initial angular velocity deviation from synchronous >> non-lock, circulation

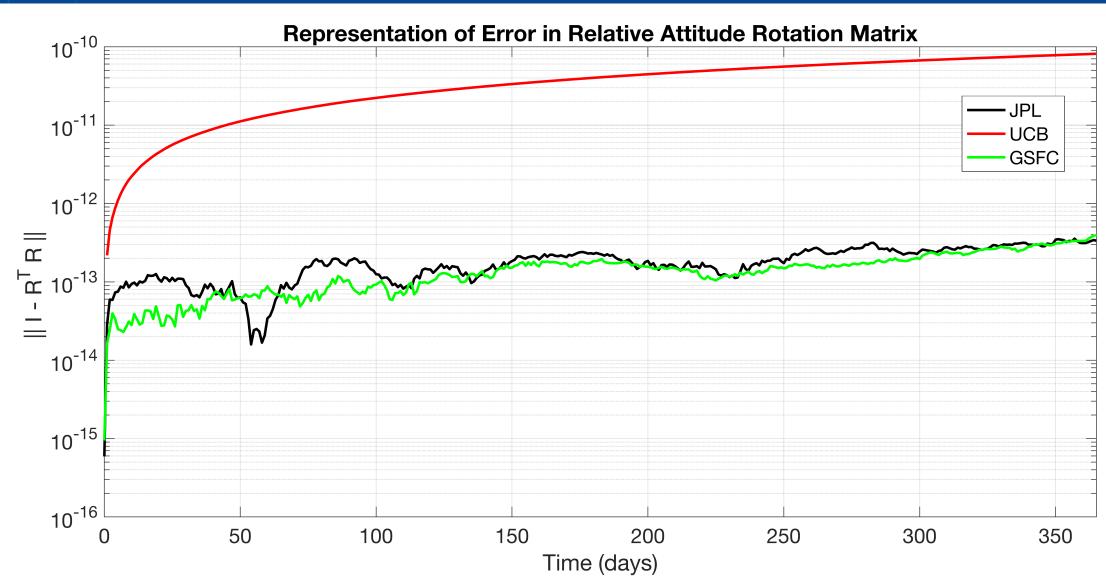




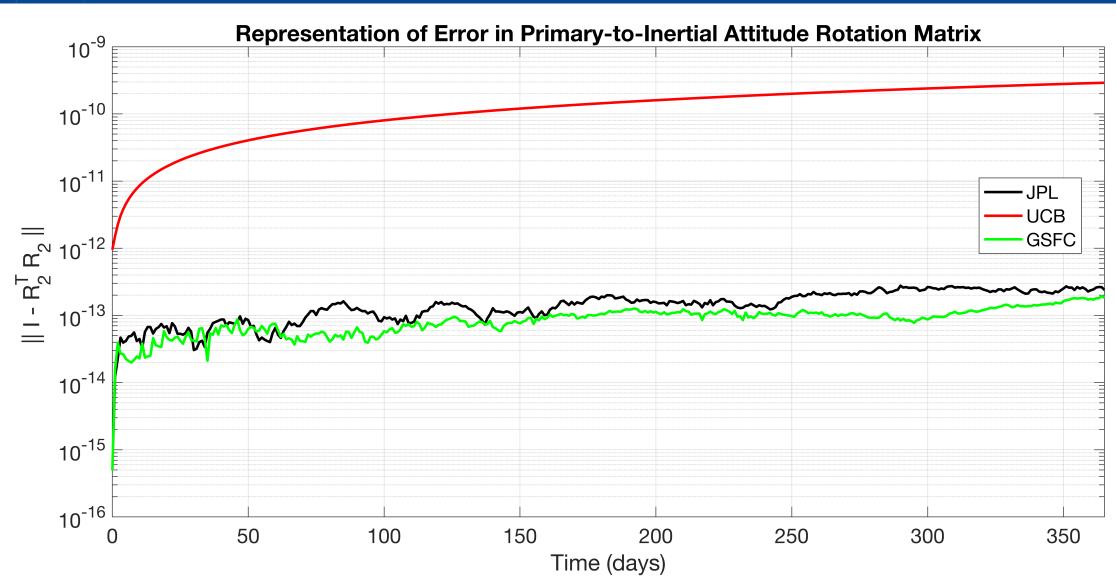




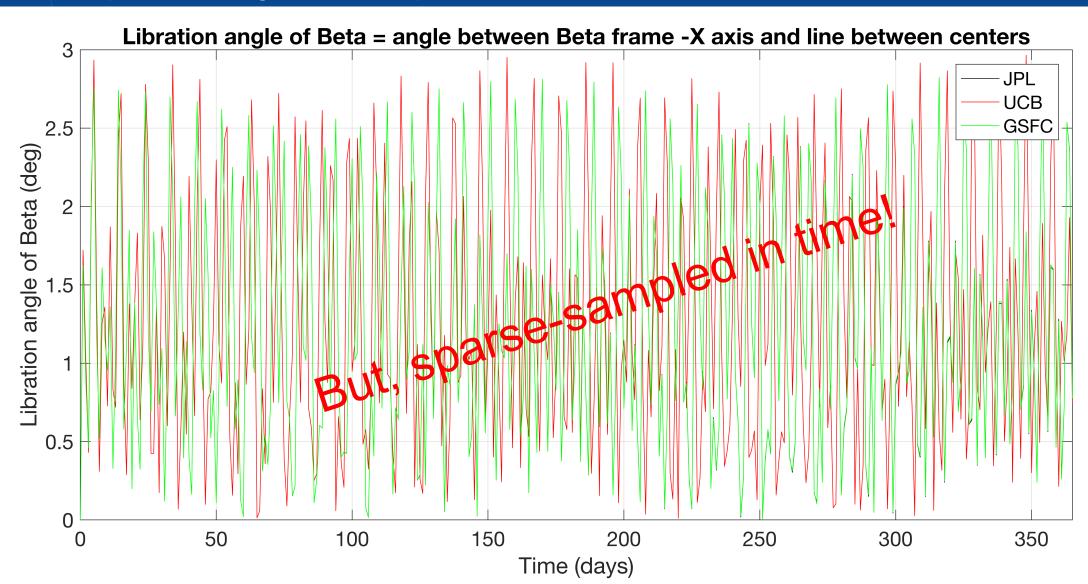
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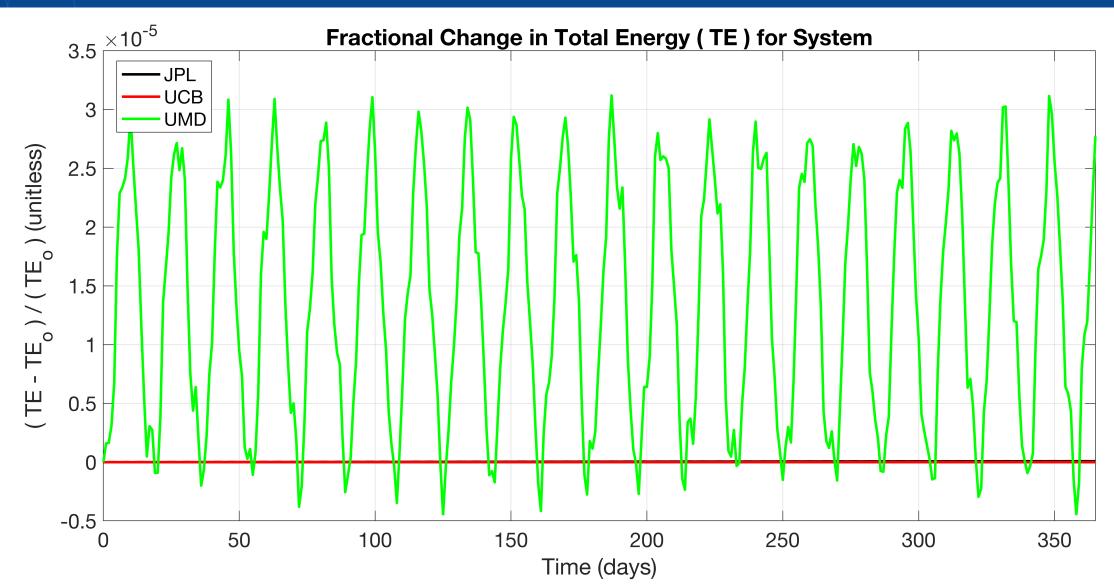


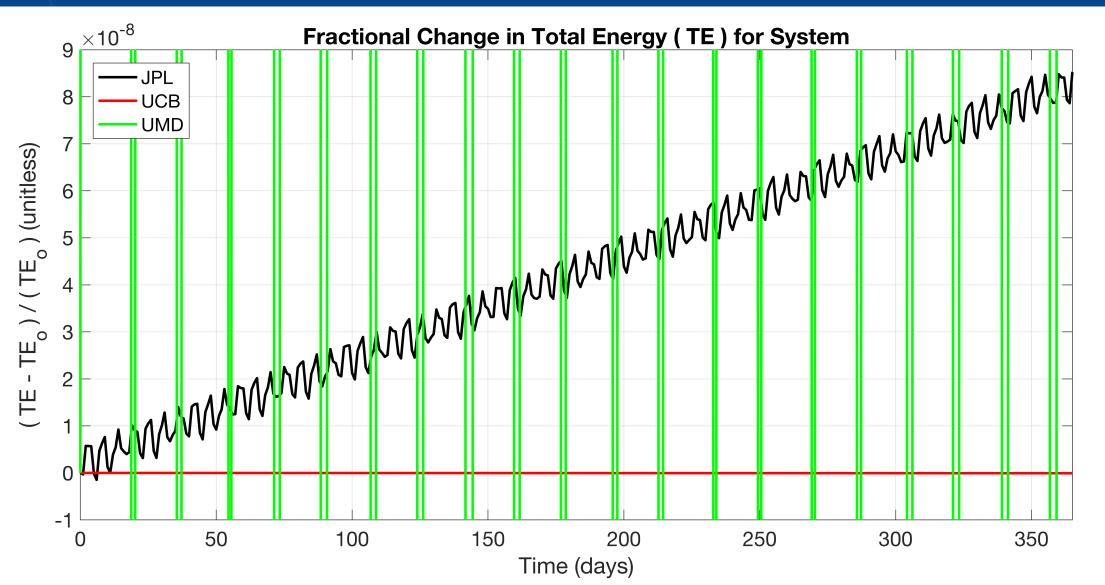
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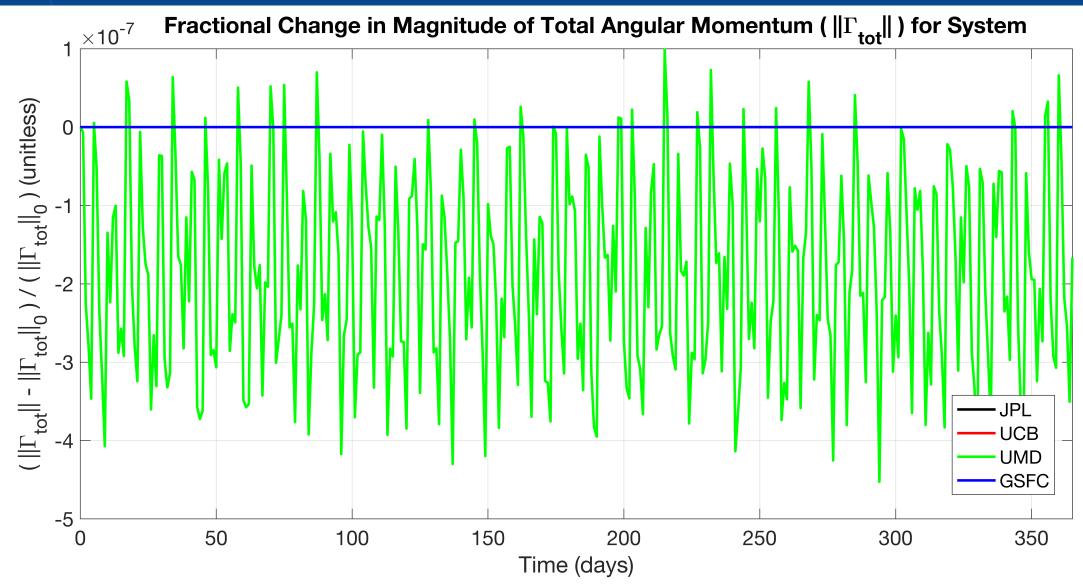


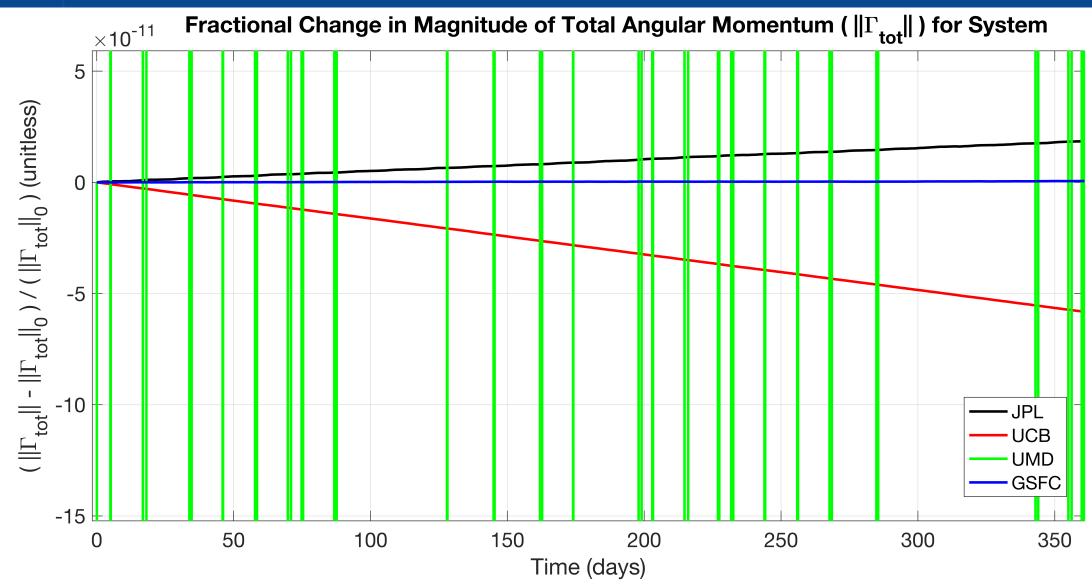
Secondary's initial angular velocity deviation >> bounded forced libration



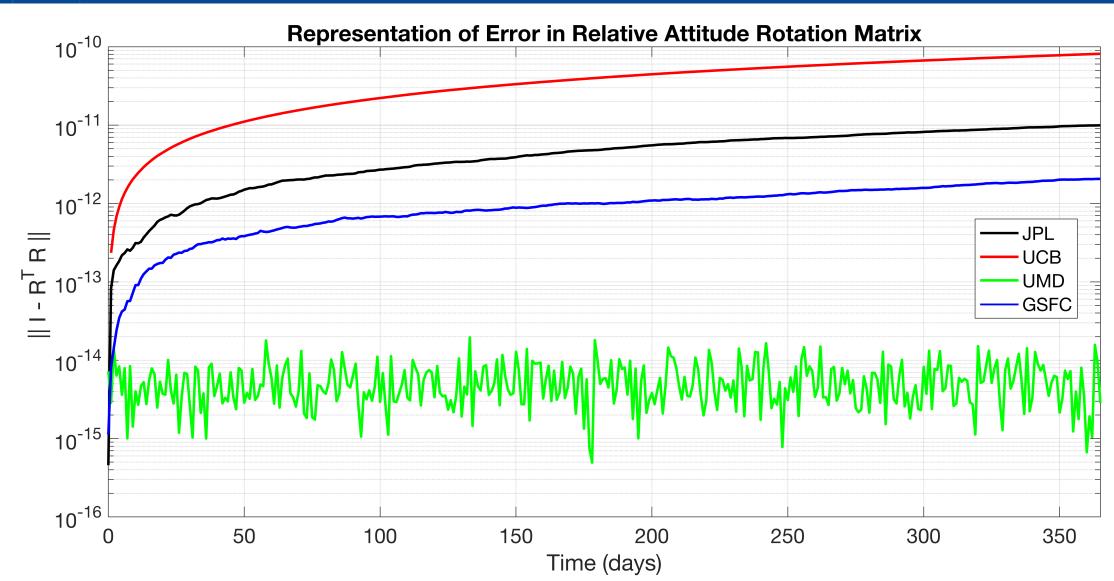




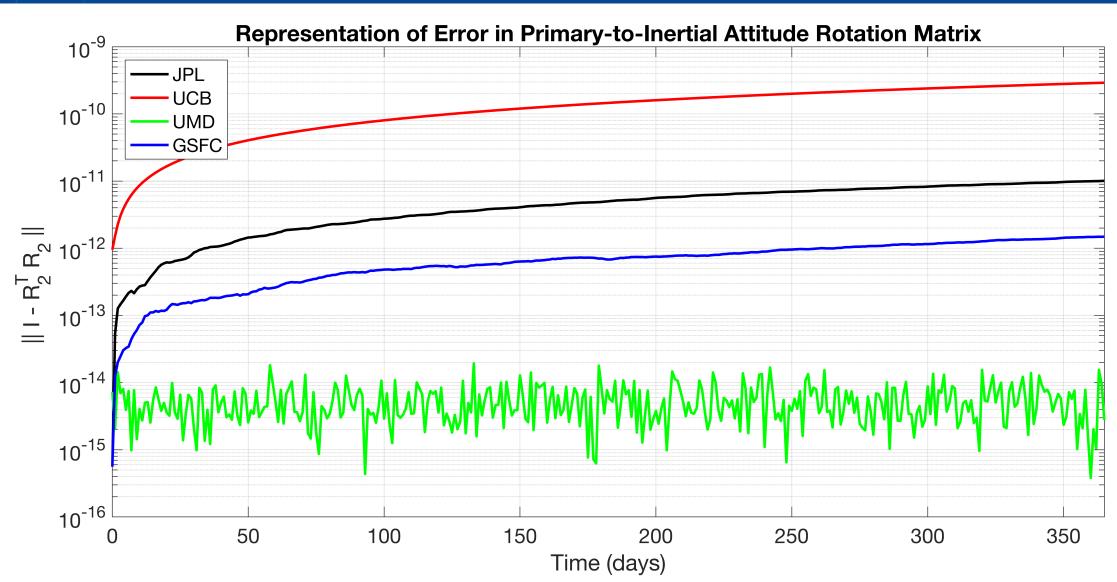




Divergence of attitude from SO(3) group, the geometry of rotational dynamics



Divergence of attitude from SO(3) group, the geometry of rotational dynamics



Benchmarking Results in Summary

Relative performance of participants, by metric, by model

Metric	Two Cubes	Two Spheres	Two Ellip.	Didymain + Ellip.
Fractional Δ in TE	UCB > AU > JPL	JPL > UCB	UCB > JPL	UCB > JPL >> UMD
Fractional Δ in TAM magnitude	JPL > GSFC > UCB > AU	JPL > GSFC > UCB	JPL > GSFC > UCB	GSFC > JPL > UCB >> UMD
$ I - R^T R $	JPL > UCB≅GSFC > AU	GSFC > JPL > UCB	JPL ≅GSFC > UCB	UMD >> GSFC > JPL > UCB
$ I - R_2^T R_2 $	JPL > GSFC > UCB > AU	GSFC > JPL > UCB	JPL ≅GSFC > UCB	UMD >> GSFC > JPL > UCB
Non-synchronous rotation or libration of secondary	JPL & UCB consistent	all are consistent	consistent in mag., not in phase	consistent in mag., not in phase

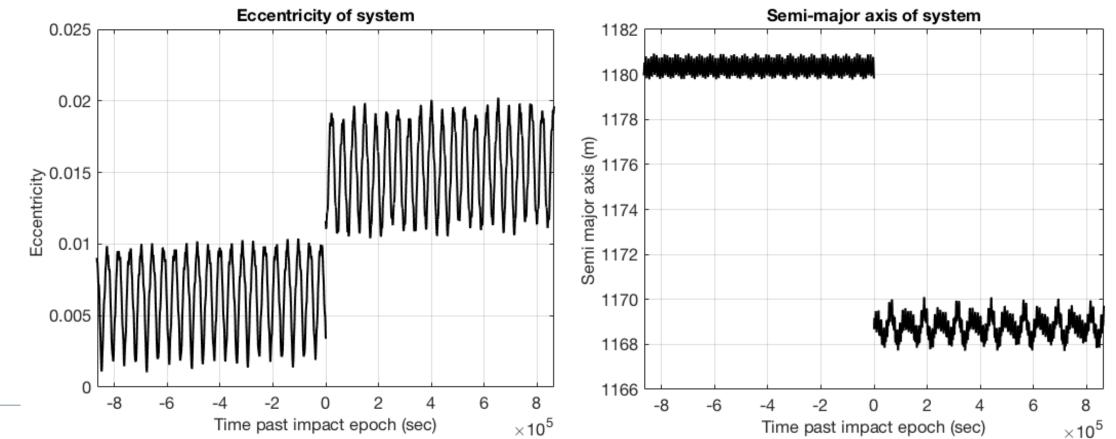
^{**} All results are highly preliminary at this stage! Analysis is ongoing



Modeling Changes Induced by DART Impact

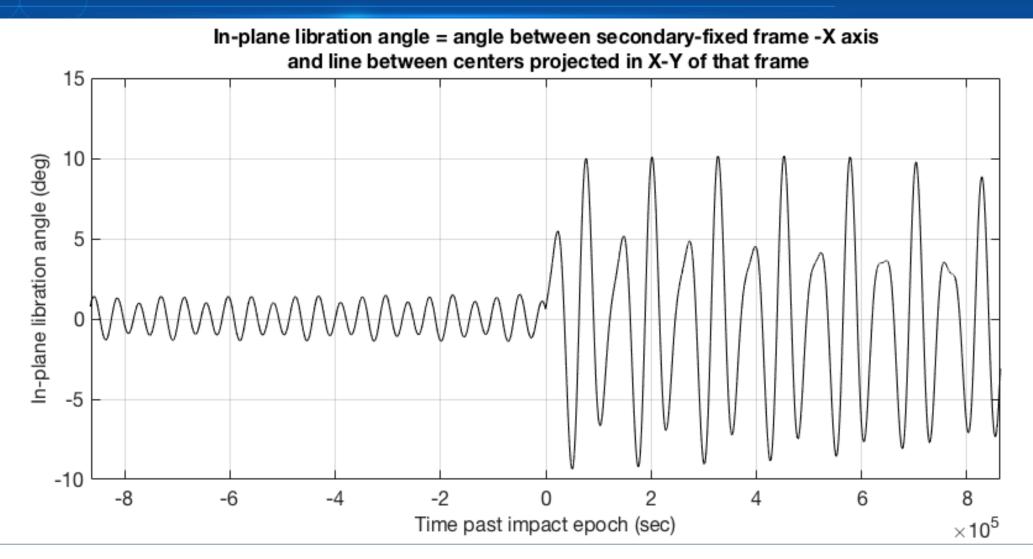
Representative Example Case

- Initial 3° misalignment of orbit pole and primary spin pole → co-precession
- Initial 0% mutual orbit eccentricity, & relaxed libration
- Momentum impulse matching $\beta = 2$ applied a little off COM...



Modeling Changes Induced by DART Impact

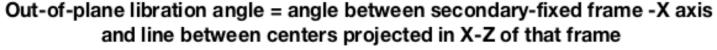
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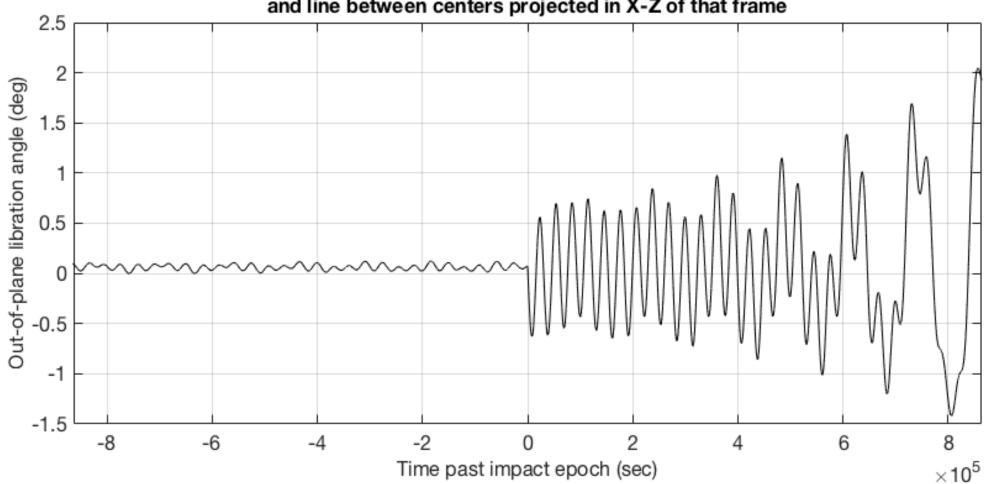




Modeling Changes Induced by DART Impact

Representative Example Case



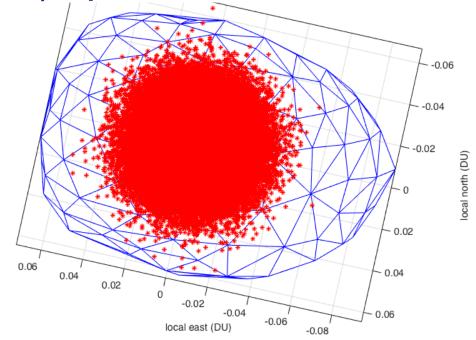




Continuing Investigations

Path Going Forward

- DART's approach relative velocity vector is essentially fixed by now
- But there exists targeting dispersion about nominal (optimal) impact location = COF
- COF itself may be offset by several meters from COM ...
- Currently β is highly uncertain ...
- We are conducting sparse raster sampling of β values and impact locations and performing F2BP simulation of post-impact dynamics in each case



Impact point dispersion on top of projection of hypothetical secondary shape into B-plane



Questions?

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